1 A Heuristic Features Selection Approach for Scenario Analysis in

# <sup>2</sup> a Regional Seismic Probabilistic Tsunami Hazard Assessment

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## 10 ABSTRACT

11 Seismic Probabilistic Tsunami Hazard Analysis (SPTHA) is aimed at estimating the annual rate of exceedance of an earthquake-induced tsunami wave of a certain location with reference to a 12 predefined height threshold. The analysis relies on computationally demanding numerical 13 simulations of seismic-induced tsunami wave generation and propagation. A large number of 14 scenarios needs to be simulated to account for uncertainties. However, the exceedance of tsunami 15 16 wave threshold height is a rare event so that most of the simulated scenarios bring little statistical contribution to the estimation of the annual rate yet increasing the computational burden. To 17 efficiently address this issue, we propose a wrapper-based heuristic approach to select the set of 18 most relevant features of the seismic model, for deciding a priori the seismic scenarios to be 19 20 simulated. The proposed approach is based on a Multi-Objective Differential Evolution Algorithm (MODEA) 21 and is developed with reference to a case study whose objective is calculating the annual rate of threshold 22 exceedance of the height of tsunami waves caused by subduction earthquakes that might be generated on a 23 section of the Hellenic Arc, and propagated to a set of target sites: Siracusa, on the eastern coast of Sicily,

- 24 Crotone, on the southern coast of Calabria, and Santa Maria di Leuca, on the southern coast of Puglia. The
- results show that, in all cases, the proposed approach allows a reduction of 95% of the number of scenarios
- 26 with half of the features to be considered, and with no appreciable loss of accuracy.
- 27 Keywords: Seismic Probabilistic Tsunami Hazard Analysis (SPTHA); Scenario selection; Feature
- 28 selection; Wrapper approach; Multi-Objective Differential Evolution Algorithm (MODEA).

#### 29 Acronyms

DF	Differential Evolution
GA	Genetic Algorithm
MODEA	Multi Objective Differential Evolution Algorithm
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NEAM	North-eastern Atlantic, the Mediterranean, and connected seas
	······································
SPTHA	Seismic Probabilistic Tsunami Hazard
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#### 30

## 31 Symbols

ā	Target site coordinates
$\psi_{ar{a}}$	Tsunami intensity in $ar{a}$
$\Delta T$	Exposure time
	Seismic scenario parameters vector
$\sigma_{ar{x}}$	Seismic scenario of parameters $\bar{x}$
Σ	Space of possible seismic scenarios
$\lambda(\sigma_{\bar{x}})$	Annual frequency of the seismic scenario $\sigma_{\! ec x}$
Pr	Probability
Pe	Probability of exceedance
$ ilde{\psi}$	Tsunami intensity threshold
$\Lambda(\psi_{\bar{a}} \geq \tilde{\psi})$	Annual frequency of occurrence of a tsunami of intensity $\psi_{ar{a}} \geq  ilde{\psi}$ at location $ar{a}$
q	Generic simulated seismic scenario
Q	Total number of seismic scenarios to be simulated
Q*	Optimised (i.e., minimum) number of seismic scenarios to be simulated
H <sub>i</sub>	Generic seismic zone

H <sub>n</sub>	Total number of seismic zones
Θ	Set of alternative ET models
θ	Generic alternative ET model
М	Number of alternative models for the calculation of $\Lambdaig(\psi_{ar{a}}\geq ilde{\psi}ig)$
<i>x</i> <sub>1</sub>	Magnitude of an earthquake
<i>x</i> <sub>2</sub>	Depth of the fault
<i>x</i> <sub>3</sub>	Strike of the focal mechanism
<i>x</i> <sub>4</sub>	Dip of the focal mechanism
<i>x</i> <sub>5</sub>	Rake of the focal mechanism
<i>x</i> <sub>6</sub>	Area of the fault
<i>x</i> <sub>7</sub>	Length of the fault
<i>x</i> <sub>8</sub>	Slip of the fault
F	Set of the objective functions of the MODEA
f	Objective function of the MODEA
Ū	Decision variable vector
$\overline{U}^*$	Solution vector
Ā	Features matrix
$ar{ar{A}}^*$	Optimal features matrix
SE	Squared error
NP	Population size of the DE
F	Scaling factor of the DE
CR	Crossover probability of the DE
MAXGEN	Maximum number of DE generations
D	Number of objectives of the MODEA

## 1. INTRODUCTION

Tsunami hazard is classically assessed by simulation of either one "worst credible" or few representative scenarios (Lorito et al. 2015; Rikitake and Aida 1988; Geist et al., 2006; Heidarzadeh et al., 2011; Gopinathan et al., 2021). This can be an effective approach when (i) the effects of 37 frequent, small magnitude earthquakes are expected to be negligible compared to those less frequent large magnitude earthquakes, and (ii) the analysis is conducted in a relatively simple 38 geophysical context where tsunami hazard is dominated by the large magnitude earthquakes 39 occurring in subduction zones, whose geometries are reasonably well constrained (Lorito et al. 40 2015). On the other hand, when tsunamis are generated in complex and fragmented tectonic 41 42 environments (e.g., the Caribbean Sea and the Mediterranean Sea) or when relatively short return periods need to be considered, the tsunami hazard might be severely biased (Lorito et al. 2015) and 43 the consequences underestimated, especially if the extent of damage is not well modelled and 44 caught (Suppasri et al., 2021). To explicitly account for the whole spectrum of seismic triggering 45 events and their related uncertainty, a probabilistic analysis of a large set of potential tsunamis can 46 47 be performed (Seismic Probabilistic Tsunami Hazard Analysis, SPTHA) (Rikitake and Aida 1988; 48 Grezio et al. 2017; Fakhruddin et al. 2021; Park et al. 2021). Specifically, SPTHA aims to estimate the probability that the height  $\psi$  of an earthquake-induced tsunami wave exceeds a threshold  $\tilde{\psi}$ , within 49 in an exposure time  $\Delta T$ , at a location of coordinates  $\bar{a}$  (Grezio et al. 2017). Each tsunami is assumed 50 to be generated by a seismic scenario  $\sigma_{\bar{x}}$  belonging to the space of possible seismic scenarios  $\Sigma$ 51  $(\sigma_{\bar{x}} \in \Sigma)$ , characterized by parameters  $\bar{x}$  and occurring with annual frequency  $\lambda(\sigma_{\bar{x}})$ . Considering a 52 Poisson process for the wave exceedance event occurrence in time, the probability of exceedance 53 54  $P_e$  can be written as:

$$P_e = Pr(\psi_{\bar{a}} \ge \tilde{\psi}; \Delta T) = 1 - exp(-\Lambda(\psi_{\bar{a}} \ge \tilde{\psi}) \Delta T)$$
(1)

55 where  $\Lambda(\psi_{\bar{a}} \ge \tilde{\psi})$  is the annual rate of occurrence of a tsunami of intensity  $\psi_{\bar{a}} \ge \tilde{\psi}$  at location  $\bar{a}$ . 56 This rate is calculated by integrating, over the space  $\Sigma$ , the annual frequency  $\lambda(\sigma_{\bar{x}})$  of occurrence of 57 the seismic scenario  $\sigma_{\bar{x}}$  times the probability  $Pr(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}})$  that the tsunami wave generated by 58 the scenario exceeds  $\tilde{\psi}$ :

$$\Lambda(\psi_{\bar{a}} \ge \tilde{\psi}) = \int_{\Sigma} \lambda(\sigma_{\bar{x}}) Pr(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}}) d\sigma_{\bar{x}}$$
<sup>(2)</sup>

59 Considering, without loss of generality and for the sake of simplicity, a set of Q discretized seismic

60 scenarios  $\sigma_{\bar{x}_q}$  (q = 1, ..., Q) with  $\lambda(\sigma_{\bar{x}_q})$  and  $Pr(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}_q})$ , Eq. (2) can be approximated as:

$$\Lambda(\psi_{\bar{a}} \ge \tilde{\psi}) \approx \sum_{q=1}^{Q} \lambda\left(\sigma_{\bar{x}_{q}}\right) Pr\left(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}_{q}}\right)$$
(3)

To account for epistemic uncertainty, M alternative formulations of  $\lambda\left(\sigma_{\bar{x}_q}\right)$  and  $Pr\left(\psi_{\bar{a}} \geq \tilde{\psi} | \sigma_{\bar{x}_q}\right)$ can be considered, producing M alternative quantifications of both factors in Eq. (3). The mean hazard rate can, then, be evaluated as:

$$\Lambda(\psi_{\bar{a}} \ge \tilde{\psi}) \approx \frac{1}{M} \sum_{m=1}^{M} \sum_{q=1}^{Q} \lambda\left(\sigma_{\bar{x}_{q}}\right)_{m} Pr\left(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}_{q}}\right)_{m}$$
(4)

64 where  $\lambda \left( \sigma_{\bar{x}_q} \right)_m$  is the generic entry of the matrix  $\overline{\lambda(\sigma_{\bar{x}})}$ :

$$\overline{\lambda(\sigma_{\bar{x}_1})}_1 = \begin{pmatrix} \lambda(\sigma_{\bar{x}_1})_1 & \cdots & \lambda(\sigma_{\bar{x}_1})_m & \cdots & \lambda(\sigma_{\bar{x}_1})_M \\ \vdots & \vdots & \vdots & \vdots \\ \lambda(\sigma_{\bar{x}_q})_1 & \cdots & \lambda(\sigma_{\bar{x}_q})_m & \cdots & \lambda(\sigma_{\bar{x}_q})_M \\ \vdots & \vdots & \vdots & \vdots \\ \lambda(\sigma_{\bar{x}_Q})_1 & \cdots & \lambda(\sigma_{\bar{x}_Q})_m & \cdots & \lambda(\sigma_{\bar{x}_Q})_M \end{pmatrix}$$
(5)

65 and  $Pr\left(\psi_{\bar{a}} \geq \tilde{\psi} | \sigma_{\bar{x}_q}\right)_m$  is the generic entry of the matrix  $\overline{Pr(\psi_{\bar{a}} \geq \tilde{\psi} | \sigma_{\bar{x}})}$ :

$$\overline{Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}})} = \begin{pmatrix} Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{1}})_{1} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{1}})_{m} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{1}})_{M} \\ \vdots & \vdots & & \vdots \\ Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{q}})_{1} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{q}})_{m} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{q}})_{M} \\ \vdots & & \vdots & & \vdots \\ Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{Q}})_{1} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{Q}})_{m} & \cdots & Pr(\psi_{\bar{a}} \ge \tilde{\psi}|\sigma_{\bar{x}_{Q}})_{M} \end{pmatrix}$$
(6)

Note that the calculation of the entries of  $\overline{Pr(\psi_{\bar{a}} \ge \tilde{\psi} | \sigma_{\bar{x}})}$  may result computationally burdensome, for example when using highly non-linear tsunami simulation models.

In the particular case of a local SPTHA for the estimation of inundation hazard curves for a small 68 target site, e.g., a refinery, high-resolution inundation simulations are needed. This requires either 69 large High Performance Computing (HPC) resources (Gibbons et al. 2020; González et al. 2009), or 70 statistical emulation (Samanidou et al., 2019), or a reduction of the number of simulations by, for 71 72 example a two-stage filtering procedure (González et al. 2009; Lorito et al. 2015; Volpe et al. 2019), 73 or training a metamodel, for example an Adaptive Kriging that mimics the behaviour of the 74 computationally demanding tsunami inundation simulator, e.g., (Bacchi et al. 2020; Di Maio et al. 75 2021).

On the other hand, when the interest is in a regional SPTHA for the estimation of inundation hazard curves for large areas, such as countries or continents, the computation is usually performed by using simplified relationships between the water elevation at the shoreline and the maximum inundation height (Gailler et al. 2018; Glimsdal et al. 2019).

The present work considers regional SPTHA and illustrates a novel approach for identifying the relevant features of the seismic scenarios and the selection of a limited number of them needed for performing the annual rate estimation with sufficient accuracy. Specifically, a Multi-Objective Differential Evolution Algorithm (MODEA) is used to select the features (Storn and Price 1997).

84 As example of practical use, we consider the estimation of the annual rate of exceedance of a threshold  $\tilde{\psi} = 1m$  of tsunami wave height, resulting from subduction earthquakes in a section of 85 86 the Hellenic Arc. To show the applicability of the approach to different target sites, we consider the propagation of the waves towards Siracusa, on the eastern coast of Sicily, Crotone, on the southern 87 88 coast of Calabria, and Santa Maria di Leuca, on the southern coast of Puglia. We consider the crustal 89 seismicity generated in the Kefalonia-Lefkada region, thus developing outside the subduction 90 interface of the Hellenic Arc (Basili et al. 2021; Selva et al. 2016); this is one of the regions considered 91 in the tsunami hazard model recently released for the North-eastern Atlantic, the Mediterranean,

and connected seas (i.e., NEAM region) (Basili et al. 2018, 2021). In NEAMTHM18, a predefined source discretization method is applied for magnitude, hypocentres, strike, dip and rake angles. Based on this, a combinatorial setting of the parameters values makes the target source area exposed to a total of  $Q_{tot} = 23272$  seismic scenarios where M = 1000 alternative models can be used for the calculation of  $\Lambda(\psi_{\bar{a}} \ge 1m)$  (Basili et al., 2021).

97 For all the target sites, a comparison is provided between the value of the mean annual rate of 98 exceedance estimated considering only the selected scenarios SPTHA and the full set of scenarios 99 SPTHA. The outcome of the comparison shows that in all cases the proposed approach allows a 100 significant reduction of the number of scenarios needed to be processed, without affecting the 101 accuracy of the estimate.

The paper is organised as follows. Section 2 presents the case study. Section 3 explains the approach
 developed. Section 4 shows the results of the application of the proposed approach to the case
 study. Conclusions are drawn in Section 5.

## 105 2. CASE STUDY

We consider the regional SPTHA for three target sites  $\bar{a}$  located on the eastern coast of Sicily (Siracusa), the southern coast of Calabria (Crotone), and Puglia (Santa Maria di Leuca), as reported in Figure 1. All targets are exposed to tsunamis triggered by crustal earthquakes occurring outside the subduction interface of the Hellenic Arc in the Kefalonia-Lefkada region (Basili et al. 2021). Earthquakes are assumed to be generated at specific epicentral locations  $H_i$  (*i*=1,..., 42, blue points in Figure 1) with different magnitudes, depths, and faulting mechanisms. Without loss of generality, the following assumptions are made:

113 i. The threshold is of  $\tilde{\psi} = 1m$  at 50m from the coastline.

114 ii. One epicentral location (black diamond in location 14, in Figure 1) is considered, since 115 the largest number Q = 721 of seismic scenarios  $\sigma_{\bar{x}}$  is available among all other 116 locations, making,  $\Lambda(\psi_{\bar{a}} \ge 1m|H_{14})$  equal to:

$$\Lambda(\psi_{\bar{a}} \ge 1m|H_{14}) \approx \frac{1}{M} \sum_{m=1}^{M} \sum_{q=1}^{Q} \lambda\left(\sigma_{\bar{x}_{q}}|H_{14}\right)_{m} \Pr\left(\psi_{\bar{a}} \ge 1m|\sigma_{\bar{x}_{q}}, H_{14}\right)_{m}$$
(7)

117 (Herein after, for the sake of readability,  $H_{14}$  will be omitted).

118 The scenarios associated with the other neighbouring areas have not been included in

119 the study due to their similarity to those of point 14 and would not have brought any

120 further significant information.

122 iii. Each  $\sigma_{\bar{x}}$  is characterised by the set of parameters  $\bar{x} = (x_1, x_2, x_3, x_4, x_5, x_6, x_7, x_8)$  (Basili 123 et al. 2021; Selva et al. 2016), whose support and values are listed in Table 1. These 124 parameters (see Figure 2 for a schematic representation) are:

125 1. *x*<sub>1</sub> Magnitude

126 2. 
$$x_2$$
 Depth (top of the fault)

127 3. 
$$x_3$$
 Strike (of the focal mechanism)

128 4. 
$$x_4$$
 Dip (of the focal mechanism)

129 5. 
$$x_5$$
 Rake (of the focal mechanism)

130 6. 
$$x_6$$
 Area (of the fault), i.e., the product of its width by its length

## 131 7. $x_7$ Length (of the fault)

132 8.  $x_8$  Slip (of the fault)

133 It is worth mentioning that all parameters are discretized to build a finite list of scenarios, in line

134 with the recommendations provided by NEAMTHM18 (Basili et. 2021): bins are defined linearly for

### all the parameters except for the magnitude for which the larger the magnitude events the finer the

discretization needed, motivated by a tsunamigenic reasons (Lorito et al. 2015, Selva et al. 2016).
Also, since the slip parameter value is dependent on the value of the magnitude (and, therefore,
and the discretization adopted), two different scaling laws (see Basili et al., 2021) are adopted for
strike and dip-slip events.

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Figure 1 – Seismic zones H<sub>i</sub> (i=1,...,42) of the Hellenic Arc (blue dots), the source considered (black diamond), the target sites ā
Siracusa (red cross), and Crotone and Santa Maria di Leuca (black crosses).

Fault projection to ground surface



145

Figure 2 – Schematic representation of an earthquake and its parameters (Basili et al. 2008).

146 Table 1 – Parameters of the seismic scenarios (Each parameter has its specific discretization, resulting in a different number of

147 reference values and bins).

[0.67-4.21]
[0.01]
0.67
0.95
1.09
1.29
1.30
1.71
1.73
2.21
2.24
2.79
2.82
3.44
3.48
4.16
4.21

## 149 3. METHODOLOGY

To alleviate the computational burden of the SPTHA, the procedure sketched in Figure 3 is 150 151 developed. Firstly, an optimisation problem is solved to identify the optimal set of seismic scenarios that contribute most to  $\Lambda(\psi_{\bar{a}} \ge 1m)$  of Eq. (7). Then, their features values are identified. The 152 optimisation is performed by a wrapper-based heuristic approach: based on a Multi-Objective 153 Differential Evolution Algorithm (MODEA) wherein the Differential Evolution (DE) engine (Reynoso-154 Meza 2021; Storn and Price 1997) iteratively searches for candidate sets of scenarios, among the 155 original dataset of Q = 721 scenarios, whose performance is evaluated with respect to a given cost 156 157 function (the interested reader may refer to Appendix A). Once the optimal set of scenarios is 158 identified, their common features are retrieved by statistical analysis.





Figure 3 – Wrapper approach for optimal set of scenarios selection based on MODEA



## 162 Step 1: Consider the original dataset

163 The original dataset  $\overline{\overline{A}} = [Q \times 9]$  is:

$$\overline{\overline{A}} = \begin{pmatrix} x_{1,1} & \cdots & x_{8,1} & \Lambda(\psi_{\overline{a}} \ge 1m | \sigma_{\overline{x}_{1}}) \\ \vdots & \vdots & \vdots & \vdots \\ x_{1,q} & \cdots & x_{8,q} & \Lambda(\psi_{\overline{a}} \ge 1m | \sigma_{\overline{x}_{q}}) \\ \vdots & \vdots & \vdots & \vdots \\ x_{1,Q} & \cdots & x_{8,Q} & \Lambda(\psi_{\overline{a}} \ge 1m | \sigma_{\overline{x}_{Q}}) \end{pmatrix}$$

$$(8)$$

where  $x_{1,q}$  is the value of the parameter  $x_1$  in the *q*-th scenario,  $x_{2,q}$  is the value of the parameter  $x_2$  in the *q*-th scenario, etc., and  $\Lambda\left(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_q}\right) = \frac{1}{M} \sum_{m=1}^{M} \lambda\left(\sigma_{\bar{x}_q}\right)_m Pr\left(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_q}\right)_m$  is the annual rate of exceedance of the *q*-th scenario.

#### 167 Step 2: Apply MODEA to identify the most relevant scenarios

The MODEA searches the global minimum of a set of objective (cost) functions  $F = \{f(\cdot)\}$ , of one (or more) decision vector(s)  $\overline{U}$  (typically a string of binary digits) (Zio, Baraldi, and Gola 2007; Zio, Baraldi, and Pedroni 2006). In the case of interest for this work,  $\overline{U}$  indicates whether the *q*-th seismic scenario is considered in the candidate solution (*q*-th bit equal to 1) or not (*q*-th bit equal to 0).

The MODEA search is performed by initially randomly sampling the bits of the *NP* vectors that compose the initial population strings (Zio et al. 2006). Then, iteratively, the population is enriched by the solution  $\overline{U}$  that best fits the objective functions, through a selection process driven by a set of parameters, i.e., the scaling factor *F* and the crossover probability *CR* (Storn and Price 1997). For a thorough description of the process based on DE and its controlling parameters, the interested reader may refer to the Appendix A or to (Storn and Price 1997).

178 The two objective functions considered are:

179 1. Minimisation of Q (i.e., the number of scenarios  $\sigma_{\bar{x}_q}$  considered in the solution):

$$f_1 = \sum_{q=1}^Q U_q \tag{9}$$

180 2. Minimisation of the squared error *SE* between the annual rate of exceedance 181  $\Lambda(\psi_{\bar{a}} \ge 1m)$  and the annual rate of exceedance calculated considering exclusively the

182 
$$Q^* = \min\left(\sum_{q=1}^{Q} U_q\right)$$
 selected scenarios  $\Lambda^*(\psi_{\bar{a}} \ge 1m)$ :

$$f_2 = \left(\Lambda(\psi_{\bar{a}} \ge 1m) - \Lambda^*(\psi_{\bar{a}} \ge 1m)\right)^2 \tag{10}$$

183 where  $\Lambda^*(\psi_{\bar{a}} \ge 1m)$  is calculated as:

$$\Lambda^*(\psi_{\bar{a}} \ge 1m) = \sum_{q=1}^Q \lambda\left(\sigma_{\bar{x}_q}\right) Pr\left(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_q}\right) U_q \tag{11}$$

The search procedure ends when the stopping criterion (e.g., the maximum number of generations
 MAXGEN) is reached.

#### 186 Step 3: Optimal set of scenarios

The optimal solution vector  $\overline{U}^*$  (i.e., the optimal set of scenarios) that optimizes the multi-objective function of Eqs. (9) and (10) is selected from the Pareto optimal front (Zio et al. 2006), as the solution with the minimum number  $Q^*$  of entries equal to 1 (i.e., the scenarios considered in the candidate solution).

#### 191 Step 4: optimal features identification

To identify the most relevant features to be considered for the SPTHA, we first calculate the optimal features matrix  $\overline{A}^* = [Q^* \times 9]$ , as the Hadamard product of the original dataset  $\overline{A}$  with  $\overline{U}^*$  (with  $(Q - Q^*)$  null vector rows):

$$\bar{\bar{A}}^* = \bar{\bar{A}} \circ \bar{U}^* \tag{12}$$

$$\bar{A}^{*} = \begin{pmatrix} x_{1,1} & \cdots & x_{8,1} & \Lambda(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_{1}}) \\ \vdots & \vdots & \vdots & \vdots \\ x_{1,q^{*}} & \cdots & x_{8,q^{*}} & \Lambda(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_{q^{*}}}) \\ \vdots & \vdots & \vdots & \vdots \\ x_{1,Q^{*}} & \cdots & x_{8,Q^{*}} & \Lambda(\psi_{\bar{a}} \ge 1m | \sigma_{\bar{x}_{Q^{*}}}) \end{pmatrix}$$
(13)

196 Then, the matrix  $\overline{A}^*$  is columnwise compared with the original dataset  $\overline{A}$  to assess their commonality 197 (i.e., the optimal features subset).

## 198 4. RESULTS

199 The approach described in Section 3 has been applied to the case study presented in Section 2. The search for optimal scenarios among the Q = 721 of the original dataset is performed by a MODEA 200 (DE/rand/1/bin strategy, see Appendix A for further details), with objective functions  $f_1$  and  $f_2$ 201 (respectively Eq. (9) and Eq. (10)), where  $f_2$  is calculated referring to the benchmark value of the 202 annual rate of exceedance  $\Lambda(\psi_{\bar{a}} \ge 1m) = 3.3193 \cdot 10^{-12} yr^{-1}$  calculated from the full set of 203 scenarios. In practice, each candidate solution  $\overline{U}$  is a binary string of Q = 721 bits. The population 204 205 size NP, the scaling factor F, the crossover probability CR and the generation bound MAXGEN, have been expertly set equal to 20, 0.5, 0.9 and 10000, respectively: specifically, NP has been set 206 equal to  $10 \cdot (\#of \ objectives = 2) = 20$  in line with (Storn and Price 1997); CR has been set equal 207 to 0.9 for a fast convergence (Storn and Price 1997); F has been set equal to 0.5 in line with (Ahmed 208 2005; Storn and Price 1997); the stopping criterion MAXGEN = 10000 has been set following a 209 trial-and-error procedure (Reynoso-Meza 2021). 210





Figure 4 – Pareto optimal front after MAXGEN iterations

213 When the stopping criterion is reached, the Pareto front shown in Figure 4 is obtained:

1.  $\overline{U}_1^*$  yields  $Q^* = 38$  scenarios with a  $SE = 8.5^{-30}yr^{-2}$  and a percentage error of 0.085% 215 2.  $\overline{U}_2^*$  yields  $Q^* = 39$  scenarios with a  $SE = 8.1^{-30}yr^{-2}$  and a percentage error of 0.066% 3.  $\overline{U}_3^*$  yields  $Q^* = 40$  scenarios with a  $SE = 8.0^{-30}yr^{-2}$  and a percentage error of 0.063%

In this work, the solution  $\overline{U}_1^*$  is preferred because it yields the minimum number of  $Q^* = 38$ 217 scenarios (i.e., a 95% reduction with respect to Q) with a reasonably small  $SE = 8.5^{-30} years^{-2}$ 218 (i.e., a percentage error of 0.085%) in the estimation of  $\Lambda(\psi_{\bar{a}} \ge 1m|H_{14})$ . In Table 2, all the features 219 and  $Q^*$  scenarios selected by the MODEA are listed (for the Siracusa target), without discarding low-220 frequency scenarios (Di Maio et al. 2021). All  $Q^*$  selected scenarios contribute to  $\Lambda(\psi_{\bar{a}} \ge 1m|H_{14})$ 221 with a relatively large probability of threshold exceedance  $\Lambda(\psi_{\bar{a}} \ge 1m|H_{14}, \sigma_{\bar{x}_q})$ . On the contrary, 222 most of the Q = 721 seismic scenarios in the original dataset have a  $\Lambda(\psi_{\bar{a}} \ge 1m, \sigma_{\bar{x}_a}) < 10^{-20}$ , 223 i.e., bring a negligible contribution to the estimation of  $\Lambda(\psi_{\bar{a}} \ge 1m|H_{14})$  but increase the 224 computational burden. Furthermore, regarding the features selected to characterise the  $Q^* = 38$ 225

scenarios, these are reduced with respect to those that characterise the Q scenarios as shown in

Table 3 and Figure 4-Figure 12.

228 For geophysical interpretation of the results obtained, we consider the independent features, i.e.,

the Magnitude and the angles of the faulting mechanism (Strike, Dip, and Rake).

230 For the remaining features, Depth, Area, Length and Slip that are dependent on the independent

231 features, a discussion is provided in the Appendix B.

**232** Table 2 – Features and  $\Lambda\left(\psi_{\bar{a}} \ge 1m|H_{14}, \sigma_{\bar{x}_q}\right)$  of the  $Q^* = 38$  selected scenarios (Siracusa target site)

<i>x</i> <sub>1</sub>	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	<i>x</i> <sub>4</sub>	<i>x</i> <sub>5</sub>	<i>x</i> <sub>6</sub>	<i>x</i> <sub>7</sub>	<i>x</i> <sub>8</sub>	$\Lambda\left(\psi_{\bar{a}} \geq 1m   H_{14}, \sigma_{\bar{x}_q}\right)$
6.5000	1.00	337.5	50	90	318.95	22.68	0.67	3.98E-17
6.8012	1.00	157.5	50	90	638.11	34.39	0.95	4.17E-16
6.8012	1.00	157.5	70	90	638.11	34.39	0.95	2.79E-16
6.8012	1.00	157.5	90	270	638.11	34.39	0.95	3.28E-16
6.8012	1.00	157.5	90	90	638.11	34.39	0.95	1.35E-16
6.8012	1.00	337.5	70	90	638.11	34.39	0.95	4.16E-17
6.8012	1.00	337.5	50	270	638.11	34.39	0.95	2.12E-17
6.8012	1.00	337.5	50	90	638.11	34.39	0.95	4.17E-16
6.8012	1.00	337.5	30	90	638.11	34.39	0.95	4.04E-13
6.8012	7.56	337.5	50	90	638.11	34.39	0.95	2.95E-16
6.8012	7.56	337.5	30	90	638.11	34.39	0.95	4.38E-13
6.8012	14.12	337.5	30	90	638.11	34.39	0.95	8.72E-15
7.0737	1.00	22.5	50	90	1194.98	50.10	1.30	2.41E-17
7.0737	1.00	157.5	50	270	1194.98	50.10	1.30	1.33E-16
7.0737	1.00	157.5	50	90	1194.98	50.10	1.30	1.50E-15
7.0737	1.00	157.5	70	90	1194.98	50.10	1.30	1.59E-15
7.0737	1.00	157.5	90	270	1194.98	50.10	1.30	1.11E-15
7.0737	1.00	337.5	70	90	1194.98	50.10	1.30	1.64E-16
7.0737	1.00	337.5	50	270	1194.98	50.10	1.30	4.02E-16
7.0737	1.00	337.5	50	90	1194.98	50.10	1.30	2.05E-15

7.07371.00337.530901194.9850.101.309.94E-137.07379.43157.570901194.9850.101.302.32E-177.07379.43337.530901194.9850.101.307.13E-137.07379.43337.510901194.9850.101.304.25E-177.32031.00157.550902108.2970.441.733.30E-167.32031.00157.570902108.2970.441.731.05E-167.32031.00157.5902702108.2970.441.731.94E-137.32031.00337.530902108.2970.441.733.45E-137.320311.58337.550902108.2970.441.733.45E-137.320311.58337.550902108.2970.441.731.48E-137.320311.58337.550902108.2970.441.731.48E-137.320311.58337.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.241.73E-177.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.241.78E-167.54351.0033	7.0737	1.00	337.5	30	270	1194.98	50.10	1.30	3.26E-17
7.07379.43157.570901194.9850.101.302.32E-177.07379.43337.530901194.9850.101.307.13E-137.07379.43337.510901194.9850.101.304.25E-177.32031.00157.550902108.2970.441.733.30E-167.32031.00157.570902108.2970.441.731.05E-167.32031.00157.5902702108.2970.441.733.45E-137.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.530902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.570903524.5595.872.241.96E-167.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.54351.00337	7.0737	1.00	337.5	30	90	1194.98	50.10	1.30	9.94E-13
7.07379.43337.530901194.9850.101.307.13F-137.07379.43337.510901194.9850.101.304.25F-177.32031.00157.550902108.2970.441.733.30F-167.32031.00157.570902108.2970.441.731.05F-167.32031.00157.5902702108.2970.441.731.94F-167.32031.00337.530902108.2970.441.733.45F-137.320311.58157.550902108.2970.441.735.44F-177.320311.58337.550902108.2970.441.735.44F-177.320311.58337.550902108.2970.441.731.48F-137.4351.00157.550902108.2970.441.731.48F-137.54351.00157.550903524.5595.872.241.96F-167.54351.00337.550903524.5595.872.241.78F-167.54351.00337.530903524.5595.872.242.51F-137.54351.00337.530905524.5595.872.242.51F-137.54351.00337.530905524.5595.872.242.51F-137.54351.00337.	7.0737	9.43	157.5	70	90	1194.98	50.10	1.30	2.32E-17
7.07379.43337.510901194.9850.101.304.25E-177.32031.00157.550902108.2970.441.733.30E-167.32031.00157.570902108.2970.441.731.05E-167.32031.00157.5902702108.2970.441.731.94E-167.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.0737	9.43	337.5	30	90	1194.98	50.10	1.30	7.13E-13
7.32031.00157.550902108.2970.441.733.30E-167.32031.00157.570902108.2970.441.731.05E-167.32031.00157.5902702108.2970.441.731.94E-167.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.0737	9.43	337.5	10	90	1194.98	50.10	1.30	4.25E-17
7.32031.00157.570902108.2970.441.731.05E-167.32031.00157.5902702108.2970.441.731.94E-167.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.530902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.241.78E-167.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.3203	1.00	157.5	50	90	2108.29	70.44	1.73	3.30E-16
7.32031.00157.5902702108.2970.441.731.94E-167.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.550902108.2970.441.731.48E-137.54351.00157.550902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.54351.00337.530903524.5595.872.242.51E-137.54351.00337.530905608.92126.692.823.83E-15	7.3203	1.00	157.5	70	90	2108.29	70.44	1.73	1.05E-16
7.32031.00337.530902108.2970.441.733.45E-137.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.530902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.241.73E-167.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.3203	1.00	157.5	90	270	2108.29	70.44	1.73	1.94E-16
7.320311.58157.550902108.2970.441.735.44E-177.320311.58337.550902108.2970.441.737.61E-177.320311.58337.530902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.247.34E-177.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.54351.00337.530903524.5595.872.242.51E-137.54351.00337.530905608.92126.692.823.83E-15	7.3203	1.00	337.5	30	90	2108.29	70.44	1.73	3.45E-13
7.320311.58337.550902108.2970.441.737.61E-177.320311.58337.530902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.241.73E-177.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.54351.00337.530905608.92126.692.823.83E-15	7.3203	11.58	157.5	50	90	2108.29	70.44	1.73	5.44E-17
7.320311.58337.530902108.2970.441.731.48E-137.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.247.34E-177.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.3203	11.58	337.5	50	90	2108.29	70.44	1.73	7.61E-17
7.54351.00157.550903524.5595.872.241.96E-167.54351.00157.570903524.5595.872.247.34E-177.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.3203	11.58	337.5	30	90	2108.29	70.44	1.73	1.48E-13
7.54351.00157.570903524.5595.872.247.34E-177.54351.00337.550903524.5595.872.241.78E-167.54351.00337.530903524.5595.872.242.51E-137.74531.00337.530905608.92126.692.823.83E-15	7.5435	1.00	157.5	50	90	3524.55	95.87	2.24	1.96E-16
7.5435       1.00       337.5       50       90       3524.55       95.87       2.24       1.78E-16         7.5435       1.00       337.5       30       90       3524.55       95.87       2.24       2.51E-13         7.7453       1.00       337.5       30       90       5608.92       126.69       2.82       3.83E-15	7.5435	1.00	157.5	70	90	3524.55	95.87	2.24	7.34E-17
7.5435       1.00       337.5       30       90       3524.55       95.87       2.24       2.51E-13         7.7453       1.00       337.5       30       90       5608.92       126.69       2.82       3.83E-15	7.5435	1.00	337.5	50	90	3524.55	95.87	2.24	1.78E-16
7.7453         1.00         337.5         30         90         5608.92         126.69         2.82         3.83E-15	7.5435	1.00	337.5	30	90	3524.55	95.87	2.24	2.51E-13
	7.7453	1.00	337.5	30	90	5608.92	126.69	2.82	3.83E-15

## 234 Table 3 – Support values of the selected scenarios (Siracusa target site)

Parameter	<i>x</i> <sub>1</sub>	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	<i>x</i> <sub>4</sub>	<i>x</i> <sub>5</sub>	<i>x</i> <sub>6</sub>	<i>x</i> <sub>7</sub>	<i>x</i> <sub>8</sub>
Values	6.5000	1.00	22.5	10	90	318.95	22.68	0.67
	6.8012	7.56	157.5	30	270	638.11	34.39	0.95
	7.0737	9.43	337.5	50		1194.98	50.10	1.30
	7.3203	1158		70		2108.29	70.44	1.73
	7.5435	14.12		90		2133.31	95.87	2.24
	7.7453					3524.55	126.69	2.82
						5608.92		

#### 236 MAGNITUDE

The DE search engine for the Siracusa site has not selected (red slices in Figure 5a)) those scenarios characterized by large magnitudes ( $x_1 = 7.7453, 8.0933$ ). Indeed, for such scenarios, the annual rates are negligible and do not bring any significant contribution to the hazard curve estimation (see Eq. (7)), even if a relatively large threshold of  $\tilde{\psi} = 1m$  at 50m is assumed. Similarly, also for the target sites of Crotone and Santa Maria di Leuca (Figure 5b) and 5c), respectively), large magnitudes are neglected. Regarding Santa Maria di Leuca, also the scenarios with magnitude  $x_1 = 6.5$  are neglected, probably due to its unfavorable position with respect to the source.





247 STRIKE

Regardless of the regional tectonic setting, some strikes are privileged over others due to their greater tsunamigenic impact. That is, the algorithm chooses scenarios based on the combination of their probability of occurrence and the effect in terms of tsunami. In fact, some strikes, those perpendicular to the source-target propagation direction, are associated with a greater probability of generating a considerable impact tsunami.

For Siracusa, the DE search engine has identified as relevant (green in Figure 6a)) those scenarios characterised by strike angle values of 22.5°, 157.5°, 337.5°. These strikes are aligned with the Hellenic subduction zone. Hence, they are both highly probable and maximize the tsunami in Siracusa, as strike directions are approximately perpendicular to the source-to-site tsunami propagation path (see Figure 1). Moving toward East, for Crotone and, even more, for Leuca (see Figure 6b) and 6c), respectively), other strikes are added to the most probable and perpendicular to the source-target direction ones: in particular, being Santa Maria di Leuca located northern to the source, all strikes are selected.





264 DIP

For Siracusa and Crotone (Figure 7a) and 7b), respectively), the DE search engine has identified as relevant all dip angles in the selected scenarios: thus, dip is not a distinguishing characteristic of the scenarios.



the orientation is associated with a less impactful hazard than Siracusa and Crotone. Indeed, a





Figure 7 – Values of the dip (green) and non-selected ones (red) in the selected scenarios; a) Siracusa, b) Crotone, and c) Santa Maria
di Leuca.

274 RAKE

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For all the target sites considered, the normal and transverse mechanisms (rake values of 90° and 276 270°) are privileged, as they are associated with a greater coseismic deformation in the component 277 linked to the deformation of the seabed useful for triggering more dangerous tsunamis.

Indeed, only scenarios with rake values of 90° and 270° have been selected (green in Figure 8). This
result is expected, since dip-slip earthquakes usually generate a significant deformation of the sea
bottom, thus generating higher tsunami waves.



282 Figure 8 – Values of the rake (green) and non-selected ones (red) in the selected scenarios; a) Siracusa, b) Crotone, and c) Santa

Maria di Leuca.

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285	Without loss of generality, as a result of the MODE selection for the target site of Siracusa, the
286	analyst may simulate the scenarios characterised by:
287	- magnitude $x_1 \in (6.5000, 6.8012, 7.0737, 7.3203, 7.5435, 7.7453)$
288	- depth $x_2 \in (1, 7.56, 9.43, 11.58, 14.12);$
289	- strike $x_3 \in (22.5, 157.5, 337.5);$
290	- dip $x_4 \in (10, 30, 50, 70, 90);$
291	- rake $x_5 \in (90, 270);$
292	- area $x_6 \in (318.5, 638.11, 1194.98, 2108.29, 3524.55, 5608.92);$
293	- length $x_7 \in (22.68, 34.39, 50.10, 70.44, 95.87, 126.69);$
294	- slip $x_8 \in (0.67, 0.95, 1.30, 1.73, 2.24, 2.82)$ .
295	These results are expected, based on the tsunamigenic capability of earthquakes (see (Grezio et al.
296	2017) and references therein). They depend both on the particular case study analysed and on the
297	specific tsunami threshold of $\psi_{ar{a}} \geq 1m$ chosen. Larger tsunami intensities, e.g., $\psi_{ar{a}} \geq 10m$ , would
298	have involved different (probably larger) magnitudes. On the other hand, the results for the Strike,
299	Dip, and Rake angles are probably more general, and they are possibly still valid for larger tsunami
300	intensities. Similar conclusions may be drawn for the other target sites Crotone and Santa Maria di
301	Leuca.
302	5. CONCLUSIONS

In this work, a novel approach for reducing the number of seismic scenarios to be considered for
 SPTHA has been presented. The approach is a wrapper-based feature selection heuristic approach
 based on MODEA. It selects the relevant features of the seismic scenarios to be simulated.

The proposed approach has been applied to a case study regarding the estimation of the annual rate of exceedance of a height threshold  $\tilde{\psi} = 1m$  of tsunami waves caused by crustal earthquakes that might be generated on the Kefalonia-Lefkada region in North-western Greece and propagated to a set of target sites on the southern coast of Italy.

The proposed approach is shown capable of significantly reducing the number of features to describe the seismic source variability and the number of scenarios to be considered in the analysis, without affecting the accuracy of the estimate of the annual rate of exceedance. A geophysical interpretation of the results has also been provided.

Further research work will be devoted to the comparison of the proposed approach to other existing methods that may be applied with similar goals, e.g., a standard disaggregation procedure (Bazzurro and Cornell 1999; Gibbons et al. 2020; Selva et al. 2016).

## 318 Appendix A. Differential Evolution

Differential Evolution (DE) is a parallel direct search method which utilizes NP D-dimensional 319 parameter vectors  $x_{i,G}$ , i = 1, 2, ..., NP as a population for each generation G. NP does not change 320 during the minimisation process. The initial vector population is chosen randomly and should cover 321 322 the entire parameter space. DE generates new vectors by adding the weighted difference between two population vectors to a third vector in an operation called "mutation". The mutated vector's 323 parameters are then mixed with the elements of another predetermined vector, the target vector, 324 to yield the so-called trial vector, in an operation referred to as "crossover". If the trial vector yields 325 a lower cost function value than the target vector, the trial vector replaces the target vector in the 326 following generation. This last operation is called selection. Each population vector has to serve 327 328 once as the target vector so that NP competitions take place in one generation. DE's basic strategy can be described as follows. 329

#### 330 Mutation

For each target vector  $x_{i,G}$ , i = 1, 2, ..., NP, a mutant vector is generated according to:

$$v_{i,G+1} = x_{r_1,G} + F \cdot \left( x_{r_2,G} - x_{r_3,G} \right) \tag{A.1}$$

with random indexes  $r_1, r_2, r_3 \in \{1, 2, ..., NP\}$ , integer, mutually different and F > 0. The randomly chosen integers  $r_1, r_2, r_3$  are also chosen to be different from the running index i, so that NP must be greater or equal to four to allow for this condition. F is a real and constant factor  $\in [0, 2]$  which controls the amplification of the differential variation  $(x_{r_2,G} - x_{r_3,G})$ .

#### 336 Crossover

In order to increase the diversity of the perturbed parameter vectors, crossover is introduced. Tothis end, the trial vector:

$$u_{i,G+1} = \left(u_{1i,G+1}, u_{2i,G+1}, \dots, u_{Di,G+1}\right) \tag{A.2}$$

339 is formed, where

$$u_{ji,G+1} = \begin{cases} v_{ji,G+1} \ if \ (randb(j) \le CR) \ or \ j = rnbr(i) \\ x_{ji,G} \ if \ (randb(j) > CR) \ and \ j \ne rnbr(i) \end{cases}$$

$$j = 1,2, \dots, D$$
(A.3)

In (A.3), randb(j) is the *j*-th evaluation of a uniform random number generator with outcome  $\in$ [0; 1]. *CR* is the crossover constant  $\in$  [0; 1] and has to be determined by the user. rnbr(i) is a randomly chosen index  $\in$  1, 2, ..., *D* which ensures that  $u_{i,G+1}$  gets at least one parameter from  $v_{i,G+1}$ .

#### 344 Selection

To decide whether or not it should become a member of generation G + 1, the trial vector  $u_{i,G+1}$  is compared to the target vector  $x_{i,G}$  using the greedy criterion. If vector  $u_{i,G+1}$  yields a smaller cost function value than  $x_{i,G}$ , then  $x_{i,G+1}$  is set to  $u_{i,G+1}$ ; otherwise, the old value  $x_{i,G}$  is retained.

The above scheme is not the only variant of DE which has proven to be useful. In order to classify the different variants, the notation: DE/x/y/z is introduced where: x specifies the vector to be mutated which currently can be "rand" (a randomly chosen population vector) or "best" (the vector of lowest cost from the current population); y is the number of difference vectors used; z denotes the crossover scheme. The current variant is "bin" (Crossover due to independent binomial experiments). Using this notation, the basic DE-strategy described can be written as DE/rand/1/bin.

This whole section is extracted from (Storn and Price 1997).

## 357 Appendix B

358 DEPTH

The DE search engine has identified as relevant mainly those scenarios characterised by a depth value of 1km, along with a few scenarios characterised by depth values of 7.56km, 9.43km, 11.58km, and 14.12km calculated in line with NEAMTHM18 documentation (Basili et al. 2018, 2021) (green in Figure 9). This result is justified by the dependence of the depth on the magnitude: a depth equal to 1km is considered for all magnitudes whereas larger depths, instead, are modelled for smaller magnitudes only, that have been found as important (see Figure 9).



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Figure 9 – Values of the depth (green) and non-selected ones (red) in the selected scenarios

#### **367** AREA

Area values are computed relying on empirical scaling relationships from magnitude (e.g. log *Area* =  $A + B \times Magnitude$ ), using different relationships for dip-slip ( $x_5 = 90^\circ, 270^\circ$ ) and strike-slip ( $x_5 = 0^\circ, 180^\circ$ ) earthquakes (Basili et al. 2008). Only the scenarios with area values of 318.5 $km^2$ , 638.11 $km^2$ , 1194.98 $km^2$ , 2108.29 $km^2$ , 3524.55 $km^2$ , 5608.92 $km^2$  (green in Figure 10) have been selected, i.e., those scenarios corresponding to small magnitude dip-slip earthquakes. In other words, larger area values, corresponding to larger magnitudes, have not been coherently
selected as well as smaller area values, corresponding to smaller magnitudes and strike-slip
earthquakes.

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Figure 10 - Values of the area (green) and non-selected ones (red) in the selected scenarios

#### 379 LENGTH

Length values are computed relying on empirical scaling relationships from magnitude (e.g. log Length =  $A + B \times Magnitude$ ), using different relationships for dip-slip ( $x_5 = 90^\circ, 270^\circ$ ) and strike-slip ( $x_5 = 0^\circ, 180^\circ$ ) earthquakes (Basili et al. 2008). Only the scenarios with length values of 22.68km, 34.39km, 50.10km, 70.44km, 95.87km, 126.69km (green in Figure 11) have been selected, i.e., those scenarios corresponding to small magnitude dip-slip earthquakes. In other words, larger length values, corresponding to larger magnitudes, have not been coherently selected as well as smaller length values, corresponding to smaller magnitudes and strike-slip earthquakes.







Figure 11 – Values of the length (green) and non-selected ones (red) in the selected scenarios

389 SLIP

Slip values are computed relying on empirical scaling relationships from magnitude (e.g.  $Slip \propto$ *Magnitude/Area*), using different relationships for dip-slip ( $x_5 = 90^\circ, 270^\circ$ ) and strike-slip ( $x_5 =$ 0°, 180°) earthquakes (Basili et al. 2008). Only the scenarios with slip values of 0.67, 0.95, 1.30, 1.73, 2.24, 2.82 (green in Figure 12) have been selected, i.e., those scenarios corresponding to small magnitude dip-slip earthquakes. In other words, larger slip values, corresponding to larger magnitudes, have been coherently selected as well as smaller slip values, corresponding to smaller magnitudes and strike-slip earthquakes.







Figure 12 – Values of the slip (green) and non-selected ones (red) in the selected scenarios

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