

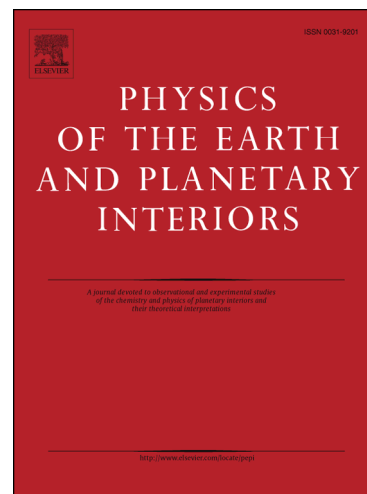
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Brittle-ductile transition depth versus convergence rate
in shallow crustal thrust faults: considerations on
seismogenic volume and impact on seismicity

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Abstract

Earthquakes occur in the Earth's crust where rocks are brittle, with magnitude increasing with the volume involved in the coseismic stage. Largest volumes are expected in convergent tectonic settings since thrust fault may be even more than 25 times larger than hypocenter depth. In general, the maximum depth of hypocenters within the crust corresponds to the brittle-ductile transition (BDT). The deepening of the BDT increases the potential seismic volume, hence raising the energy released during an earthquake. Here, by means of 2-D thermo-mechanical modelling dedicated to intraplate thrusts and thrusts within fold-and-thrust belts (shallow crust), the deepening of the BDT depth in convergent settings with variable convergence rates is investigated. Results of models characterized by shallow faults (15°- 20° dip) show that BDT depth deepens by 15 km increasing the convergence rate from 1 to 10 cm/yr. Steeper thrust faults (25°- 40° dip) show a lower

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degree of deepening of the BDT ($\simeq 5$ km) as convergence rate is increased. Calculated BDT depths allow the calculation of maximum seismic volumes involved during thrust earthquakes. Deeper BDT depths obtained assuming higher convergence rates imply larger seismic volumes and an increase of 2 orders of magnitude of the stored potential energy, as effectively observed in nature.

Keywords: Thrust fault earthquakes, Continental crust, Seismic volume, Brittle-ductile transition depth, Convergence rate

1. Introduction

Compressional earthquakes mainly occur at convergent plate boundaries where the highest magnitudes and most shallow earthquakes have been recorded (Figure .1a). Released seismic energy scales with fault dimension [e.g., 1, 2, 3, 4] - and therefore with the rock volume involved during the coseismic stage [5, 6, 7, 8] - and with convergence rate [9, 10, 11].

The seismogenic volume is constrained by the fault length and the depth of the brittle-ductile transition (BDT) or the depth of the decollement layer [12]. Bird and Kagan (2004) [13] found that plate boundaries are associated with earthquakes characterized by seismic moment resulting from different thicknesses of coupled seismogenic lithosphere. The distribution of earthquake hypocenters gives a first approximation of the seismogenic thickness, and hence of the maximum depth of faulting [14]. For earthquakes with magnitude $M_w > 5$ worldwide [15], earthquakes foci deepen where the largest events have been recorded ($M_w > 8.5$), ranging in depth from 25 to 50 km and almost coinciding with convergent plate boundaries regions (e.g., Sumatra,

17 Japan, Chile). Shallower hypocentral depths (<25 km) typify divergent and
18 strike-slip margins where rarely $M_w > 8$. Furthermore, thrust faults display
19 higher ratios between fault length and hypocenter depth (up to more than
20 25) with respect to strike-slip and normal faults (around 10 and 3 respec-
21 tively). This implies that thrusts are associated with the largest volumes
22 activated at the coseismic stage [5].

23 A distinction may be made between shallow crustal and subduction-
24 interface thrust earthquakes that differ in terms of tectonic loading mecha-
25 nisms [e.g., 16]. Interplate ruptures at subduction interfaces [17], that release
26 the largest part of seismic moment in convergent margins, evolve following a
27 peculiar deformation cycle [18, 19] and respond to peculiar scaling laws relat-
28 ing magnitude and geometric/kinematics parameters [e.g., 20, 21]. Intraplate
29 thrusts and thrusts within fold-and-thrust belts (shallow crustal) deliver a
30 significant 20 to 30 % of the seismic energy budget and more evidently depend
31 on the convergence rate [22].

32 While rupture-scaling relationships are routinely used in seismic hazard
33 studies, (non)linear relations between relative plate velocity and seismicity
34 rate or moment rate or maximum possible magnitude are harshly debated and
35 considered true [11, 23, 24, 9, 10] or not [25, 26, 27] depending on assumptions
36 and data selection [e.g., 28, 29]. Uncertainties derive also from the short
37 period of global instrumental observations [10, 26, 30].

38 The lower boundary of the seismogenic layer reaches maximum depths of
39 about 40 km [31, 32]. A comparison of convergence rates from GPS data (see
40 Appendix A) with seismogenic depths extrapolated from available regional
41 studies indicates that the faster the convergence, the thicker this seismogenic

42 layer (Figure .1b and Table 1). For convergent plate margins, minimum
43 seismogenic layer thicknesses (10-15 km) occur in slowly (0-2 cm/yr) conver-
44 gent realms (Calabrian Arc [33, 34, 35], Apennines [14], Aegean and Zagros
45 [36, 37]). Such thickness values increase to around 20 km in intermediate
46 (4-6 cm/yr, i.e. India [37]) convergent settings. Although the focus of this
47 work is not on megathrusts in subduction zones, the increase of seismogenic
48 layer thickness with convergence rate applies also to these realms, as shown
49 in figure .1 by the behavior of subduction zones characterized by intermedi-
50 ate (5-7 cm/yr, i.e. Cascadia [38, 39], Sumatra[39, 40, 41] and Chile [42])
51 and fast (up to 10 cm/yr, i.e. Japan [39, 43]) convergence.

52 Here, the relationship between convergence rate and BDT deepening is in-
53 vestigated by 2D thermo-mechanical models of shallow crustal thrust faults.
54 Searching for the BDT depth values and considering homogeneous litholo-
55 gies, the brittle-ductile behavior of rocks is evaluated depending on applied
56 convergence rate in compressional tectonic regimes. In addition to the con-
57 trol provided by convergence rate, the effects of other parameters, i.e. the
58 thermal structure of the domain [e.g., 44], and the viscous limit on strength
59 [e.g., 45] are tested as well. Modelling results are used to calculate the avail-
60 able seismic volumes and predict the potential stored energy that may be
61 released during an earthquake.

62 **2. Modelling strategy**

63 Implementing models to predict the location of the BDT for increas-
64 ing/decreasing convergence rate is not a straightforward task. In fact, the
65 BDT depth is not constant since it depends on a number of factors, including

66 geothermal gradient (i.e., temperature), strain rate, stress regime, pore-fluid
67 pressure and grain size [46, 47, 48, 49]. Rock strength profiles show that at
68 relatively low temperatures and pressures (depth lower than 10-20 km) the
69 crust is brittle. Strength of rocks linearly increases with depth under the con-
70 trol of the stress regime and fluid pressure [50, 51]. The buildup of deviatoric
71 stress creates the condition to trigger earthquakes that occur once friction
72 is overcome. For a rock of given mineralogical composition and rheologi-
73 cal parameters, increasing convergence rates are associated with increasing
74 strength, hence larger differential stresses can be supported as strain rate
75 increases. An increase in temperature with depth favors plastic deformation
76 mechanisms. Ductile strength decreases exponentially with depth and stress
77 relaxes due to aseismic creep [52, 46, 47]. The switching point from brittle
78 slip to creep at depth is defined as the brittle-ductile transition (BDT) [53]
79 and it corresponds with the maximum differential stress supported by rocks
80 in their stability field (Figure .2b).

81 The 2D numerical model was created using the thermo-mechanical code
82 LAPEX-2D [54, 55]. This software permits modelling of realistic temperature-
83 and stress-dependent viscoelastic rheology combined with Mohr-Coulomb
84 plasticity [56]. At each calculation step (6.12×10^{-4} kyr), the algorithm
85 automatically selects the more appropriate rheology (elasto-plastic or non-
86 linear visco-elastic) at the current conditions of temperature and strain rate
87 (see reference [54] for detailed description of the algorithm and the choice of
88 time step value). The model allows evaluation of rheological profiles through
89 the variation of convergence rates as initial boundary condition. Modelled
90 geometries describe a 2D portion of wet-quartzitic upper crust 250 km wide

91 and 40 km thick, cut by a fault with different dip values in the range of
 92 15-40 degrees (Figure .2a). Grid resolution is 1×1 km. The non-Newtonian
 93 power-law viscosity (η) is calculated as

$$\eta = \left(\frac{1}{2}\right)B^{-1/n}(\varepsilon_{II})^{1/n-1}exp(Q/(nRT))d^m \quad (1)$$

94 where B , n and Q are parameters, ε_{II} is the second invariant of strain rate,
 95 R is the gas constant, d^m (with $m=0$ [57]) is the grain size and T is the
 96 temperature [54]. Implemented rheological parameters are from [58] and
 97 listed in Table 2. The initial temperature distribution of the reference model
 98 grows from 0 °C at the surface up to 500 °C at the bottom of the domain (40
 99 km depth) following a steady state continental geotherm [59]. To test effects
 100 of the local geothermal gradient, the temperature at the bottom was varied
 101 between 400 and 600 °C (Figure .2c), i.e. within the typical range at 40 km
 102 depth within the continental lithosphere [60].

103 According to previous studies [61, 62, 63] the fault decoupling is simulated
 104 via a 2 km thick weak zone, whose weakness is obtained assuming a lower
 105 friction angle and cohesion within the fault domain. Sensitivity of results
 106 to fault friction angle (3 to 30 degrees), cohesion (0 to 10 MPa [64]) and
 107 grain size of the domain (1 to 3 mm) are shown (Figure .2c). Shortening is
 108 simulated via fixed velocities at the left boundary of the model. Hydrostatic
 109 pressure is applied at the bottom while other boundaries are left free. A
 110 set of models was run for all considered fault dip values (15-40 degrees) and
 111 assuming convergence rates varying between 1 and 10 cm/yr. The model
 112 evolution time is 100 kyr providing that the steady state of the solution is
 113 largely achieved.

114 3. Results

115 Figure .3a presents the calculated strain rate after 50 kyr of shortening
116 at 1 cm/yr (upper panel) and 10 cm/yr (lower panel) respectively, for a
117 reference model considering a 20 degrees dipping fault. Both results show
118 that strain focuses along the fault zones with rates of $10^{-13} s^{-1}$ and $10^{-12} s^{-1}$
119 on average. The faster the convergence rate, the deeper the deformation
120 zone propagates (down to 10 km and to 20 km). The point of the model
121 that records the maximum value of differential stress (purple stars in Figure
122 .3a) is assumed as the location of the brittle-ductile transition depth for that
123 solution. Plotting BDT depths vs their location for all the models, it can be
124 recognized a transition band (pink area in Figure .3b) that includes the whole
125 set of BDT points obtained with our calculations for the reference model.
126 The transitional band is laterally delimited by the faults traces with steeper
127 (40°) and shallower (15°) dip angles. Top and bottom limits are isolines,
128 which combine the points of maximum differential stress obtained by models
129 characterized by shortening rates of 1 cm/yr (up) and 10 cm/yr (down)
130 respectively. It is evident that, depending on the shortening rate, BDT
131 depths increase from minimum values of 4-8 km (at 1 cm/yr) to maximum
132 values of 16-18 km (at 10 cm/yr). This range of variation is very sensitive to
133 the fault geometry being larger for shallow dip faults (Figure .3b and S1). In
134 fact, the upper limit occurs at depths of 4 km, 9 km and 13 km in case of fault
135 dipping 15° , 20° or 25° respectively, while the lower limit moves upward from
136 18 km to 16 km depths increasing the dip angle to 25° . In case of steeper
137 (25° - 40°) faults the range of the resulting BDT depths becomes steady (12-
138 17 km). Results show low sensitivity to parameters variation (Figure .3c).

139 The BDT depths remain comparable to those obtained with the reference
140 model if the grain size for the domain (from 1 to 3 mm) or the fault strength
141 (i.e., cohesion from 0 to 10 MPa) are increased. Results are more sensitive
142 to the initial temperature profile (shallower BDTs are obtained assuming
143 cooler crust) and to the friction angle (narrower and shallower BDT depth
144 for increasing angle) assigned to the fault especially at slow convergence rates
145 (see error bars in figure .3c).

146 4. Discussion

147 The results of numerical models dedicated to contractional tectonic set-
148 tings with variable convergence rates show that the faster the convergence,
149 the deeper the BDT (Figure .3a). A ten times faster shortening (from 1
150 to 10 cm/yr) generates a doubling of the BDT depth (from 10 to 20 km).
151 This BDT depth variation is mainly controlled by the thermal structure of
152 the crust that results for increasing convergence rates. Faster convergence
153 produces lower temperatures at depth. Lower temperature at depth induces
154 deeper BDT (figure .3c). These values are consistent with observations from
155 fold-and-thrust belts and intraplate contractional areas. As examples, in re-
156 gions characterized by convergence rates of few mm/yr like Emilia (Italy)
157 (that experienced a seismic sequence in 2012 [65]) or the New Madrid seis-
158 mic zone [66], brittle deformation is confined at depths of 10-15 km. This
159 value fits the depth of the decollement constrained by geological data for
160 both the N-Apennines [67] and the New Madrid area [68], although they
161 belong to different tectonic systems (fold-and thrust belt and intraplate re-
162 gion respectively). The BDT depth decreases up to few kilometers for even

163 smaller shortening rates (Figure S2). Where the India plate converges with
164 Eurasia at rates of 4-6 cm/yr, the BDT is well defined at depth of 15-16
165 km [69, 70]. Intraplate earthquakes around the descending oceanic plate at
166 the Japan plate boundary (converging at 10 cm/yr) illuminate a seismogenic
167 volume down to 25 km [71], comparable with the $\simeq 20$ km obtained from our
168 models.

169 Unlike earthquakes due to extensional tectonics operating in favor of grav-
170 ity (graviquakes [5]), the physics behind earthquakes in thrust settings (elas-
171 toquakes) requires much more energy to activate the process. In fact, thrust
172 earthquakes not only need to overcome the static friction over the fault but
173 enough energy to lift up the involved seismic volume is also required. More-
174 over, the fault length/depth ratio (hence the volume) increases moving from
175 normal ($\simeq 3$) to strike-slip ($\simeq 10$) and thrust faults ($\simeq 25$) [5]. This ex-
176 plains why the largest magnitudes worldwide are recorded at convergent plate
177 boundaries (Figure .1a).

178 Deeper BDT depths imply larger brittle volumes that have to be mo-
179 bilized by tectonic processes (Table 3), and thus necessitate greater energy
180 storage; the deeper the BDT, the larger the magnitude of the expected earth-
181 quake. The seismogenic depth-convergence rate relationship highlighted in
182 this work allows calculation of the volumes potentially involved during the
183 coseismic slip (grey prism in Fig. .4). The distance from the frontal thrust
184 to the internal conjugate margin ((i.e., the width W in Figure .4) is derived
185 assuming that the frontal thrust and the conjugate fault are perpendicular.
186 The volume length (L_f in figure .4) is assumed to be 25 times the BDT
187 depth. Following the approach in [6] the brittle volume (V_b) is defined from

188 BDT depth (z_{bdt}), fault dip (α) and rupture length (L_f) as:

$$V_b = L_f \left(\frac{3}{2} z_{bdt}^3 [\cot(\alpha) + \cot(90 - \alpha)] \right) \quad (2)$$

189 BDT depth and fault dips are those from calculations. Considering low
 190 angle faults dipping at 15°- 20°, involved volumes grow very fast from $\simeq 3$ -
 191 $4 \times 10^4 \text{ km}^3$ at 1 cm/yr to $\simeq 15$ - $19 \times 10^4 \text{ km}^3$ at 10 cm/yr (see table 3). In
 192 case of faults dipping in the range of 25°- 40°, calculated volumes increase
 193 slowly but considerably by $2 \times 10^4 \text{ km}^3$ with convergence rate. Overall,
 194 depending on the convergence rate, an increase of the volume involved during
 195 a seismic event between $2 \times 10^4 \text{ km}^3$ and $10 \times 10^4 \text{ km}^3$ can be predicted for
 196 thrust faults. This volume increase is remarkable if we consider that the
 197 slip of 10^5 km^3 of rocks could potential produce a $M_w > 8.0$ earthquake [5, 6].
 198 Available empirical relationships correlating seismic volumes and earthquakes
 199 magnitude [7, 8] allow to derive a magnitude increase of between 1 and 2 times
 200 with BDT deepening 5-15 km (Figure .5).

201 Using relationship (1) and assuming a steep thrust (with a dip of 40°), a
 202 doubling of the BDT depth, obtained increasing convergence rate from 1 to 10
 203 cm/yr, is associated with an eightfold increase of the volume (BDT 10 km =
 204 mobilized volume 25.000 km^3 ; BDT 20 km = mobilized volume 200.000 km^3).
 205 Shallow dip (dip of 15°) thrusts are characterized by larger distance between
 206 the hypocenter and the conjugate backstop, with a significant increment of
 207 the volume (e.g., BDT at 10 km = mobilized volume of 50.000 km^3 ; BDT at
 208 20 km = mobilized volume of 400.000 km^3 ; Figure .5 and table 3).

209 This value may diminish considering that the transition between creeping
 210 and locked portions of thrusts does not necessarily coincide with the BDT.

211 Also local variations in the fault parameters could affect this value (Figure
212 .3c). In particular, it could be shallower when evaporitic layers behave as
213 decollement or when shaly layers have mineralogy that may control the dif-
214 ferential frictional behavior, e.g. the Ca-smectite transformation in illite, or
215 other lithological variations that may further control the behavior of regional
216 thrust planes [72].

217 It is worth mentioning that the geometries resulting from thrust prop-
218 agation are generally considered to be controlled by mechanical properties
219 of rocks or to fault geometry [73, and references therein]. Shortening rate
220 here analyzed could also be a primary factor. For slow convergence, blind
221 thrusts and small co-seismic slips are expected to occur. In this case, fault
222 propagation at depth is possibly associated with a fault propagation fold [74]
223 at the surface (Figure .6a). Blind faults are typical in regions characterized
224 by convergence rates of few mm/yr, like Italy [75, 76]. At fast convergence
225 rates (i.e., 10 cm/yr like Japan [39, 43]) thrust faults propagate to the surface
226 involving larger portion of the fault [77]. In this case, fault bend faults [78]
227 are passively generated due to undulations in the fault plane (Figure .6b).

228 5. Conclusions

229 Comparing GPS data and available regional studies it is observed that the
230 seismogenic layer (delimited at depth by the BDT) thickens with increasing
231 convergence rates. This trend is confirmed by 2D thermo-mechanical models
232 of thrust faults, showing that BDT depths double (from 7-8 km up to 15
233 km) when increasing convergence rate from 1 to 10 cm/yr. In addition to
234 convergence rate, the BDT depth depends on the initial temperature profile

235 and on rheological assumptions (e.g., the fault friction angle).

236 BDT depths obtained from our calculations were used to derive the max-
237 imum brittle volume that may be mobilized during seismic events. This also
238 depends upon convergence rate. A doubling of the BDT depth is associated
239 with a four- to eight-fold increase of the seismogenic volume depending on the
240 fault dip, i.e., an increase of 1-2 in magnitude of the associated earthquake.
241 These results are consistent with global seismic data that show a linear in-
242 crease between convergence rates and earthquake magnitude for earthquakes
243 nucleated along plate-boundary thrust faults.

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251 results are available in the journal data repository and upon request from the
252 corresponding author.

253 **Appendix A - Method for GPS velocities**

254 Concerning figure .1, the convergence rates between plate pairs along
255 transects (black lines) were obtained from the most recent kinematic mod-
256 els and velocity solutions. Those involving the Pacific plate are obtained
257 from the Euler poles and rotation rates provided by [80], Table 2, which
258 contains the angular velocities for all the assumed rigid plates included
259 in the Global Strain Rate Model (v.2.1). They are listed relative to the
260 Pacific plate, which is the models reference plate. From this model we
261 have computed the corresponding convergence rates between the follow-
262 ing plate pairs: Pacific- North America (Alaska), Pacific-Eurasia (Japan),
263 Pacific-Australia (north and south Tonga). The convergence rate between
264 Juan de Fuca and North America plates (Cascadia) was computed using
265 the additive property of the Euler vectors, each one known with respect to
266 the Pacific plate. A second set of convergence rates was computed from
267 the GPS velocity solutions provided by [81, 82, 83] by removing the Eu-
268 ler rigid rotation of one plate with respect to the other for the following
269 plate pairs; Adria-Eurasia (Alps, north Apennines), Africa-Eurasia (Cal-
270 abrian Arc), Nazca-South America (Chile), Anatolia-Africa (Hellenic Arc),
271 India-Eurasia, Australia-Eurasia (Java-Sumatra) and Arabia-Eurasia (Za-
272 gros). All the rates best represent the inter-seismic relative plate velocity
273 around the area of transects, since they are free from seismic and post-seismic
274 non-linear behaviors; they have only a local validity since they are obtained as
275 projection of spherical motion on the tangent plane. The rates are reported
276 without uncertainties as they are not directly derived from measurements
277 (Table 1).

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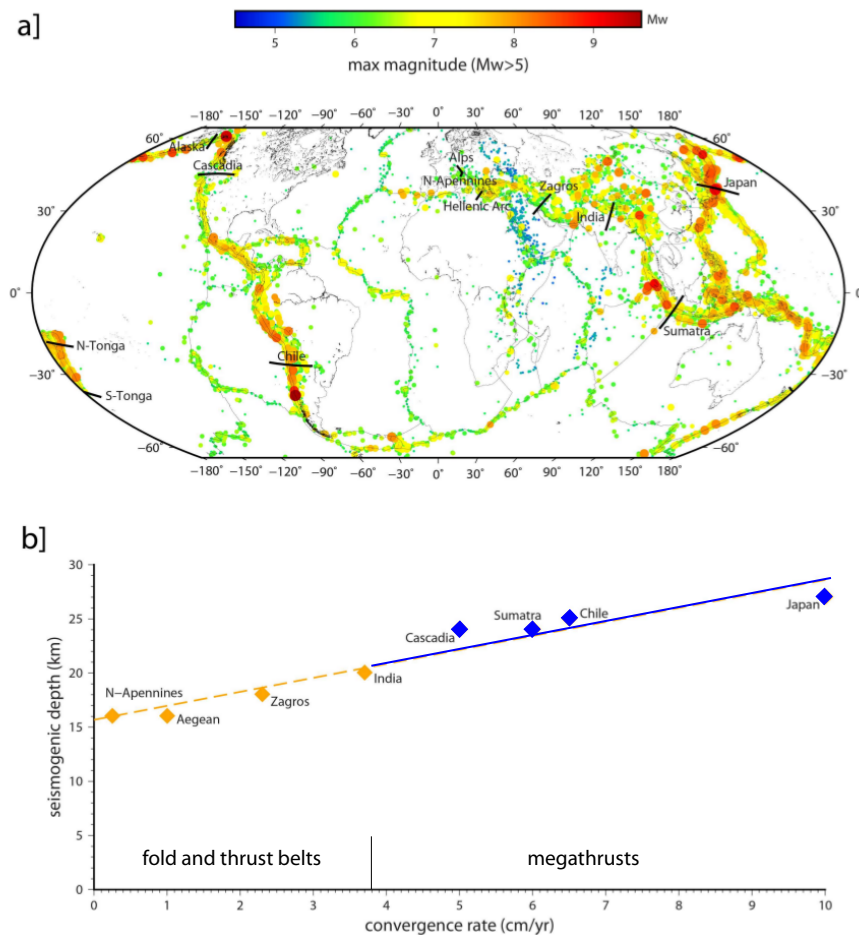


Figure 1: a) Map showing geographical distribution and magnitude of the global earthquakes ($M > 5$) for the period 1900-2013 from the ISC-GEM catalog update of January 2017 (version 4.0) [15]. Black lines represent transects where convergence rates across selected plate boundaries were calculated (appendix A) and plotted versus maximum seismogenic depths in panel b). Note that the locations of the largest earthquakes (orange-red dots in panel a)) correspond to realms characterized by higher rates of convergence. Panel b): the maximum seismogenic depth increases from 15 km at slowly converging regions (1-4 cm/yr) in fold and thrust belts (yellow diamonds) down to 25 km along faster converging boundaries (5-10 cm/yr) at subduction boundaries (blue diamonds).

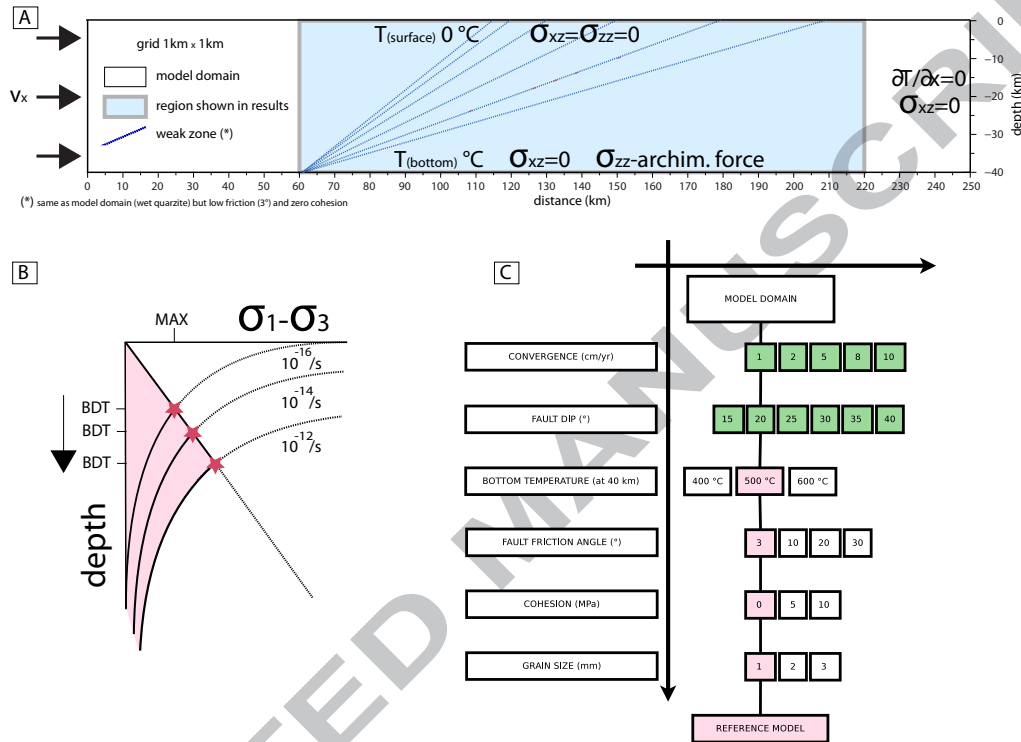


Figure 2: **Setup of numerical models.** **A]** Geometry and boundary conditions (see the main text for description). **B]** Panel showing the brittle-ductile transition (BDT) depth (purple star) defined by the point of maximum differential stress and depending on the applied strain rate. **C]** Diagram showing the range of variation for different parameters utilized in the model. Pink and green boxes highlight parameters utilized in the reference model (see table 2). Our modelling strategy requires that only one sensitivity parameter (white boxes) per run was changed with respect to reference parameters (pink boxes). All simulations provide results for each test parameter (green boxes).

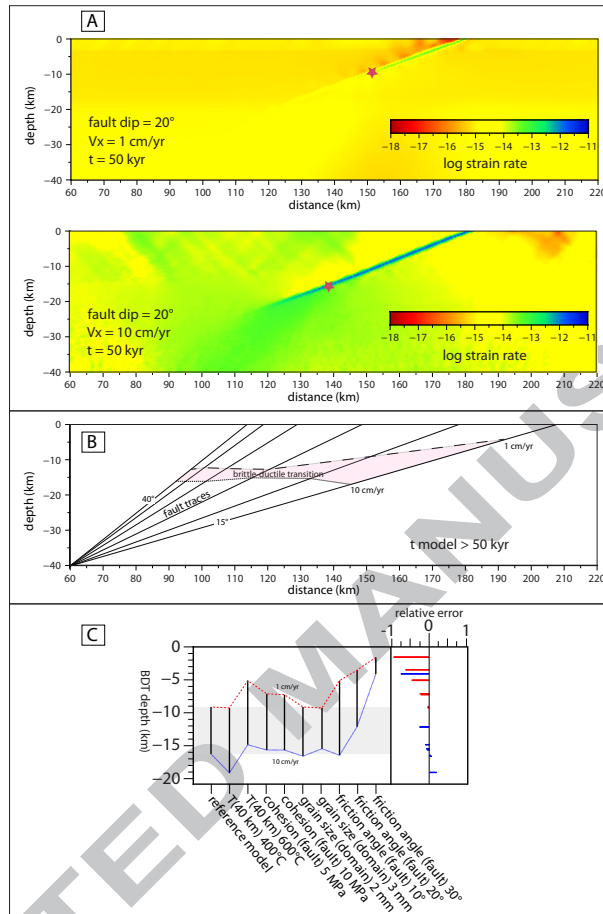


Figure 3: **Main results of numerical models.** **A]** Results of reference model showing the strain rate after 50 kyr considering a 20° dipping fault and forcing a convergence rate of 1 cm/yr (upper panel) and 10 cm/yr (lower panel). The brittle-ductile transition (BDT) depth (purple star) corresponds to the point of maximum differential stress of the model (Figure .2b) and deepens along the fault (area of maximum strain rate) by increasing the convergence rate (BDT at 10 km and at 20 km for rates of 1 cm/yr and 10 cm/yr respectively). **B]** Distribution of BDT depths (pink area) from results of the whole set of models with reference parameters values (pink boxes in figure .2c)). Notice that beside convergence rate, fault dip controls the range of variation of the BDT depth values being greater for shallow dipping faults (depth varies until $\simeq 12$ km if the fault dips 15° and $\simeq 5$ km if the fault dips 40° depending on forced convergence rate). **C]** Results obtained varying the sensitivity parameters and comparison with BDT depths calculated at different convergence rates for the reference model (gray area). Corresponding relative errors are also shown in red and blue for results obtained assuming 1 and 10 cm/yr of convergence respectively.

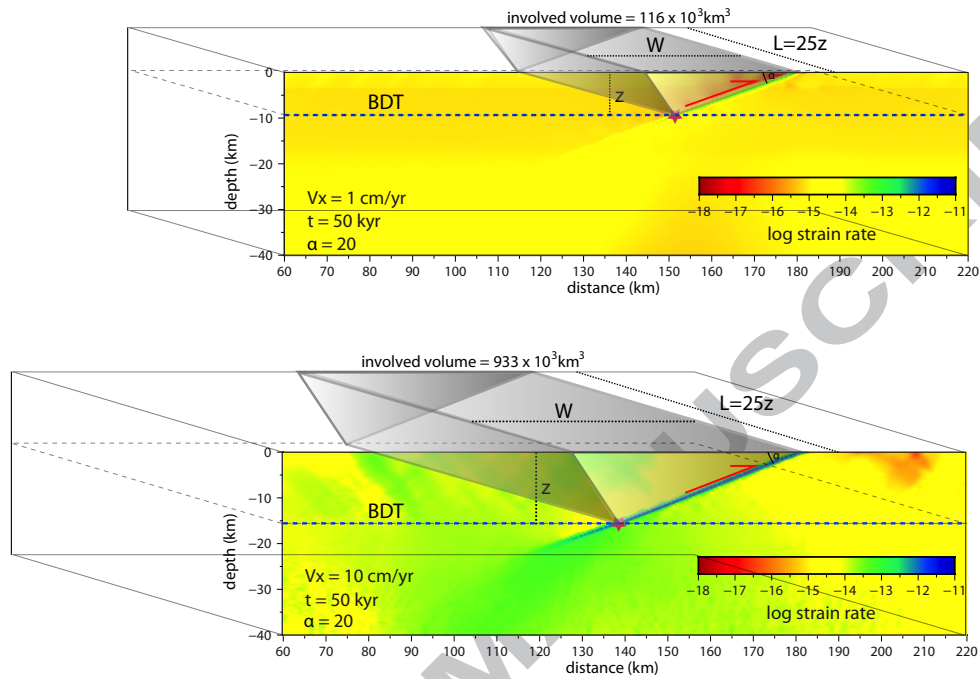


Figure 4: Sketch showing the volume involved in thrust faults earthquakes depending on BDT depth, hence on convergence rate. The doubling of the BDT depth determines an increase of the volume of at least four times, corresponding to an increase of 2 orders of magnitude of the released energy.

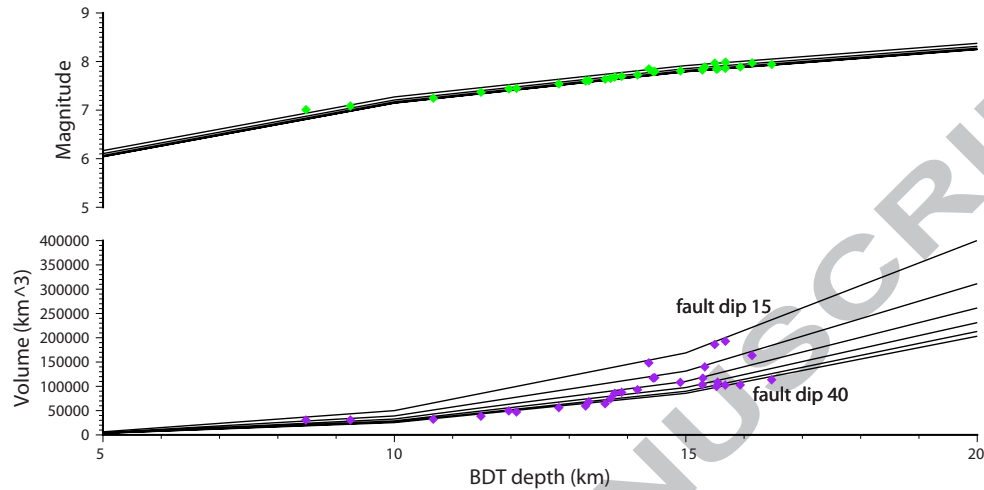


Figure .5: **BDT depth vs seismic volume and magnitude.** The volume theoretically mobilized during thrust earthquakes (lower panel) is calculated from the BDT depth using the equation in [6] for different fault dips. The related magnitudes (upper panel) are calculated with the equation proposed in [8] and show an increase of 2 when the BDT depth deepens from 5 km to 20 km. Purple and green diamonds refer to BDT depths obtained with our models. Notice that magnitude is more sensitive to BDT rather than to fault dip changes.

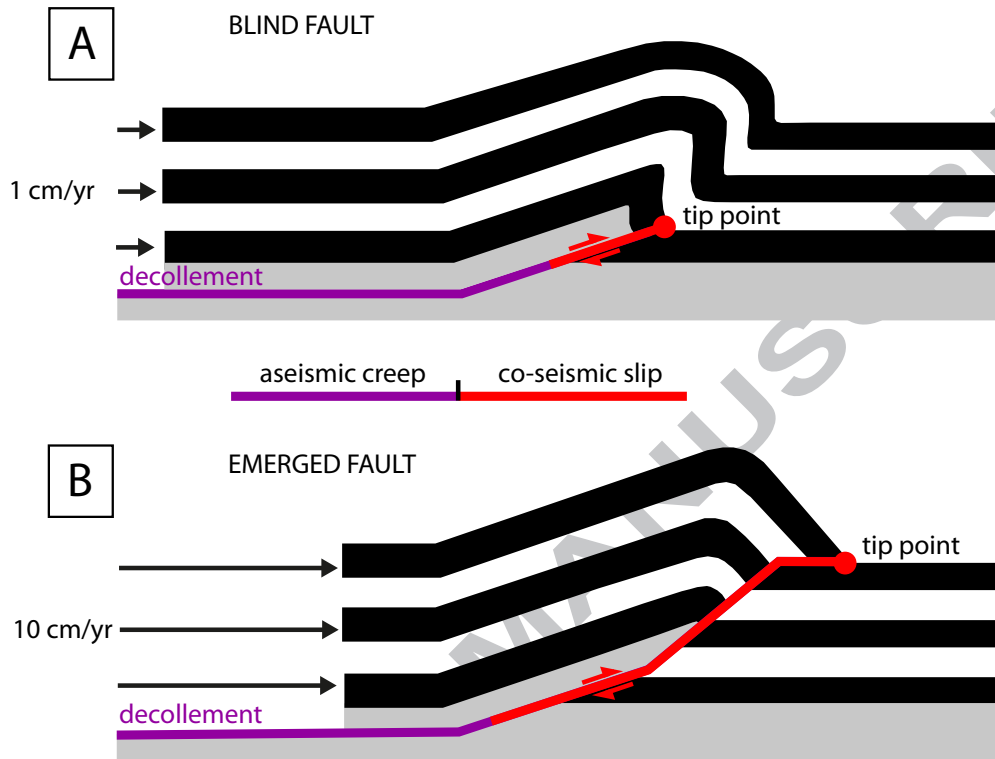


Figure .6: **Thrust-related geometries in slow and fast convergence realms.** **A]** At slow convergence rates, the small amount of co-seismic slip generates a blind thrust whereas deformation is accommodated at shallower depths by the development of a fault propagation fold. **B]** At fast convergence rates, the thrust failure propagates to the surface and a fault-bend-fold is passively generated.

subduction	rate (mm/yr)	plate pairs	source ref.
Alps	2.0	AD-EU	51
N-Appennines	2.5	EU-AD	51
Calabrian Arc	5.0	AF-EU	51
Hellenic Arc	34.0	AN-AF	52
Zagros	23.0	AR-EU	52
India	37.0	IN-EU	52
Java-Sumatra	60.0	AU-EU	53
Tonga S	49.0	AU-PA	54
Tonga N	76.0	AU-PA	54
Japan	100.0	EU-PA	54
Alaska	58.0	NA-PA	54
Cascadia	50.0	JF-NA	54
Chile	65.0	NZ-SA	53

563

564 **Table 1.** Convergence rates calculated along transects shown in Figure 1.

parameter		unit	value
density (at 20°C and 1 bar)	ρ	kg/m^3	2800
thermal expansion	α	K^{-1}	3.7×10^{-5}
bulk modulus	K	GPa	55
shear modulus	G	GPa	36
heat capacity	C_p	$J/kg/K$	1200
heat conductivity	λ	$W/K/m$	2.5
heat productivity	A	$\mu W/m^3$	1.5
creep activation energy	Q	kJ/mol	223
pre-exponential multiplier	$\log(B)$	$Pa^{-n} s^{-1}$	-28
power-law exponent	n		4
Mohr-Coulomb elasto-plasticity			
domain: friction angle		$^\circ$	30
cohesion		MPa	10
weak zone: friction angle		$^\circ$	3
cohesion		MPa	0

566 **Table 2.** Values and parameters used in the reference model.

dip	vel. (mm/yr)	$\sigma_1 - \sigma_{3max}$ (MPa)	BDTz (km)	V (km ³)	M
15	1	91.9	4.4	4361	6.0
20	1	126.2	9.2	30750	7.1
25	1	239.2	15.3	116777	7.9
30	1	259.5	15.3	103098	7.8
35	1	277.4	15.7	102567	7.9
40	1	295.3	16.5	113546	7.9
15	2	199.3	8.5	30536	7.0
20	2	262.9	15.3	140074	7.9
25	2	428.6	13.8	85462	7.7
30	2	335.0	13.3	68497	7.6
35	2	312.0	12.1	47103	7.4
40	2	345.7	13.3	59516	7.6
15	5	437.1	14.4	148301	7.8
20	5	432.0	16.1	163516	8.0
25	5	394.5	14.2	92944	7.7
30	5	348.5	12.0	49472	7.4
35	5	359.7	10.7	32307	7.2
40	5	356.6	11.5	38484	7.4
15	8	466.8	15.5	186182	8.0
20	8	392.6	14.4	117149	7.8
25	8	392.1	13.9	87698	7.7
30	8	415.4	13.7	74417	7.7
35	8	396.6	12.8	56107	7.5
40	8	417.1	13.6	64116	7.6
15	10	502.1	15.7	192864	8.0
20	10	428.1	14.5	117844	7.8
25	10	397.1	14.9	108192	7.8
30	10	437.1	15.5	108550	7.9
35	10	432.8	15.5	99663	7.8
40	10	447.9	15.9	102758	7.9

567

568 **Table 3.** Principal out-comings from numerical models and derived
569 quantities. Columns show fault dip angle, convergence rate, differential
570 stress at BDT, BDT depth, calculated seismogenic volume and potential
571 magnitude derived from seismogenic volume.